

Time integration of nonsmooth mechanical systems with unilateral contact. Conservation and stability of position and velocity constraints in discrete time.

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A naive projection scheme

A projection/activation scheme

Conclusions & Perspectives

NonSmooth Multibody Systems

Scleronomous holonomic perfect unilateral constraints

$$\begin{cases} M(q(t))\dot{v} = F(t, q(t), v(t)) + G(q(t)) \lambda(t), \text{ a.e} \\ \dot{q}(t) = v(t), \\ g(t) = g(q(t)), \quad \dot{g}(t) = G^{T}(q(t))v(t), \\ 0 \leq g(t) \perp \lambda(t) \ge 0, \\ \dot{g}^{+}(t) = -e\dot{g}^{-}(t), \end{cases}$$

where $G(q) = \nabla g(q)$ and *e* is the coefficient of restitution.

Unilateral constraints (unilateral contact, Signorini condition)



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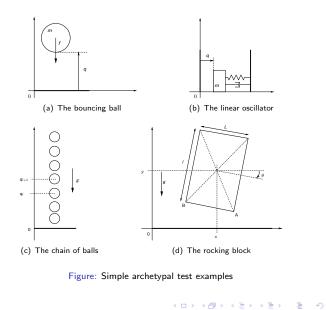
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NonSmooth Multibody Systems (NSMBS)

Academic examples



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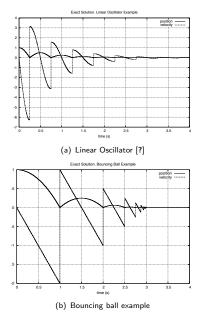
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Mechanical systems with contact, impact and friction

Simulation of Circuit breakers (INRIA/Schneider Electric)





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Mechanical systems with contact, impact and friction Simulation of the ExoMars Rover (INRIA/Trasys Space/ESA)



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SQC

State-of-the-art

Numerical time-integration methods for Nonsmooth Multibody systems (NSMBS):

Nonsmooth event capturing methods (Time-stepping methods)

- \oplus robust, stable and proof of convergence
- ⊕ low kinematic level for the constraints
- ⊕ able to deal with finite accumulation
- \ominus very low order of accuracy even in free flight motions

Two main implementations

- Moreau–Jean time–stepping scheme
- Schatzman–Paoli time–stepping scheme

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Moreau's Time stepping scheme [??]

Principle

$$M(q_{k+\theta})(v_{k+1} - v_k) - hF_{k+\theta} = p_{k+1} = G(q_{k+\theta})P_{k+1}, \quad (2a)$$

$$q_{k+1} = q_k + hv_{k+\theta}, \quad (2b)$$

$$U_{k+1} = G^T(q_{k+\theta})v_{k+1} \quad (2c)$$

$$0 \leq U_{k+1}^{\alpha} + eU_k^{\alpha} \perp P_{k+1}^{\alpha} \geq 0 \quad \text{if} \quad \bar{g}_{k,\gamma}^{\alpha} \leq 0$$

$$P_{k+1}^{\alpha} = 0 \quad \text{otherwise} \quad (2d)$$

with

- $\theta \in [0, 1]$ $x_{k+\theta} = (1-\theta)x_{k+1} + \theta x_k$ $F_{k+\theta} = F(t_{k\theta}, q_{k+\theta}, v_{k+\theta})$
- $\bar{g}_{k,\gamma} = g_k + \gamma h U_k, \, , \gamma \ge 0$ is a prediction of the constraints.

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Schatzman's Time stepping scheme [?]

Principle

$$M(q_k+1)(q_{k+1}-2q_k+q_{k-1})-h^2F_{k+\theta}=p_{k+1},$$
 (3a)

$$v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h},\tag{3b}$$

$$\left(-p_{k+1}\in N_{\mathcal{K}}\left(\frac{q_{k+1}+eq_{k-1}}{1+e}\right),$$
(3c)

where N_K defined the normal cone to K. For $K = \{q \in \mathbb{R}^n, y = g(q) \ge 0\}$

$$0 \leq g\left(\frac{q_{k+1} + eq_{k-1}}{1+e}\right) \perp \nabla g\left(\frac{q_{k+1} + eq_{k-1}}{1+e}\right) P_{k+1} \geq 0 \qquad (4)$$

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Comparison

Shared mathematical properties

- Convergence results for one constraints
- Convergence results for multiple constraints problems with acute kinetic angles
- No theoretical proof of order

Mechanical properties

- Position vs. velocity constraints
- Respect of the impact law in one step (Moreau) vs. Two-steps(Schatzman)
- Linearized constraints rather than nonlinear.

But

These schemes do not satisfy both the position and velocity constraints in discrete time.

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Objectives

Design nonsmooth event capturing (time-stepping) methods with

- ▶ Same properties as standard methods (robustness, accumulation, ...)
- Controlled drift of the constraints also for the perfect bilateral constraints
- Study of multi-body systems with clearances. (Influence of clearance on stability, avoiding violations of the same of order of clearances)
- Consistency with CAD tool and detection collision engines (which suffer even from slight violations)

Means

Projection algorithms onto the manifold defined by the constraints

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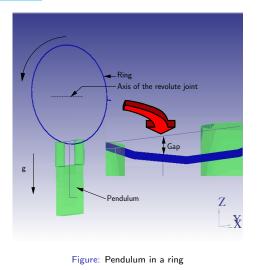
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Illustrations

Pendulum in a ring



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