

Higher order schemes for nonsmooth mechanical systems.

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General definition

$$\left\{ \begin{array}{l} M(q)\dot{v} = F(t, q, v) + G(t, q)\lambda \quad (1a) \\ \dot{q} = v \quad (1b) \\ w = g(t, q, v) \quad (1c) \\ 0 \in S(w, \lambda, t) + T(w, \lambda, t) \quad (1d) \\ v^+ = \mathcal{F}(v^-, q, t) \quad (1e) \end{array} \right.$$

- ▶ $S : \mathbb{R}^{m \times m} \times \mathbb{R} \mapsto \mathbb{R}^{m \times m}$ continuously differentiable mapping
- ▶ $T : \mathbb{R}^{m \times m} \times \mathbb{R} \rightsquigarrow \mathbb{R}^{m \times m}$ multivalued mapping with a closed graph.

Various modelling

The definition includes the modelling of Mechanical systems with bilateral constraints, Coulomb's friction, impacts, cohesion, ...

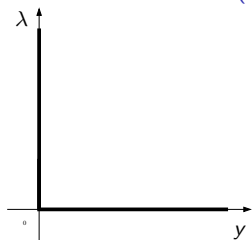
NonSmooth Multibody Systems (NSMBS)

Particular case: Scleronomous holonomic perfect unilateral constraints

$$\begin{cases} M(q)\dot{v} = F(t, q, v) + G(q)\lambda \\ \dot{q} = v \\ y = g(q) \\ 0 \leq y \perp \lambda \geq 0 \\ \dot{v}^+ = -e\dot{y}^- \end{cases} \quad (2)$$

where $G(q) = \nabla g(q)$

Unilateral constraints (unilateral contact)



Mathematical aspects (in a nutshell).

Velocity level formulation. Index reduction

$$\begin{aligned} 0 \leq y \perp \lambda \geq 0 \\ \Updownarrow \\ -\lambda \in N_{\mathbb{R}^+}(y) \\ \Updownarrow \\ -\lambda \in N_{T_{\mathbb{R}^+}}(\dot{y}) \\ \Updownarrow \\ \text{if } y \leq 0 \text{ then } 0 \leq \dot{y} \perp \lambda \geq 0 \end{aligned} \quad (3)$$

Standard assumptions

- ▶ The proper mathematical formulation is a Measure Differential inclusion (MDI)
- ▶ The position $q(t)$ is absolutely continuous function of time t
- ▶ The velocity $v(t)$ is a function of Bounded Variations (BV) of time t
- ▶ The acceleration is defined as a differential measure dv associated with the BV function v
- ▶ The multiplier is also differential measure denoted by $d\lambda$

More details in (Glocker, 2001 ; A. and Brogliato, 2008).

Compact MDI formulation (Moreau, 1988)

$$M(q)dv = F(t, q, v^+)dt + G(q)d\lambda \quad (4)$$

$$y = q(q), \dot{y} = G(q)v \quad (5)$$

$$-d\lambda \in N_{T_{\mathbb{R}^+}}(\dot{y}^+ + e\dot{y}^-) \quad (6)$$

Comments

- ▶ *The inclusion concerns measures.* Therefore, it is necessary to define what is the inclusion of a measure into a cone.
- ▶ *The inclusion in terms of velocity* v^+ rather than of the coordinates q .

Interpretation

- ▶ Inclusion of measure, $-d\lambda \in K$

- ▶ Case $d\lambda = \lambda' dt = f dt$.

$$-f \in K \quad (7)$$

- ▶ Case $d\lambda = p_i \delta_i$.

$$-p_i \in K \quad (8)$$

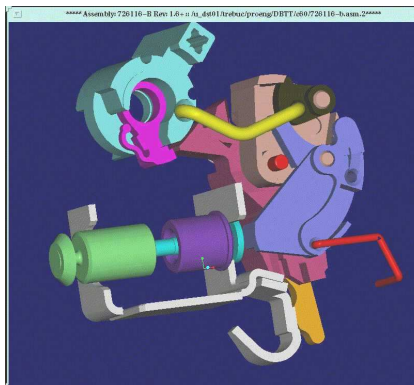
- ▶ Inclusion in terms of the velocity. **Viability Lemma**

If $q(t_0) \in C(t_0)$, then

$$v^+ \in T_C(q), t \geq t_0 \Rightarrow q(t) \in C(t), t \geq t_0$$

→ The unilateral constraints on q are satisfied. The equivalence needs at least an impact inelastic rule.

Mechanical systems with contact, impact and friction Simulation of Circuit breakers (INRIA/Schneider Electric)



Mechanical systems with contact, impact and friction

Bipedal Robot INRIA BIPOP



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Numerical time-integration methods for Nonsmooth Multibody systems (NSMBS):

Nonsmooth event capturing methods (Time-stepping methods)

- ⊕ robust, stable and proof of convergence
- ⊕ low kinematic level for the constraints
- ⊕ able to deal with finite accumulation
- ⊖ very low order of accuracy even in free flight motions

Nonsmooth event tracking methods (Event-driven methods)

- ⊕ high level integration of free flight motions
- ⊖ no proof of convergence
- ⊖ sensibility to numerical thresholds
- ⊖ reformulation of constraints at higher kinematic levels.
- ⊖ unable to deal with finite accumulation

Objectives & means

Higher order schemes for nonsmooth mechanical systems.

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Objectives

Design nonsmooth event capturing methods with

- ▶ same properties as standard methods (robustness, accumulation, ...)
- ▶ Higher resolution (ratio error/computational cost)
- ▶ Higher order of accuracy

Means

1. Adaptive time-step size and order strategies for standard methods
2. Mixed integrators with rough pre-detection of events
3. Splitting strategies
4. Ad hoc detection of discontinuity and order of discontinuity methods.

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Academic examples I

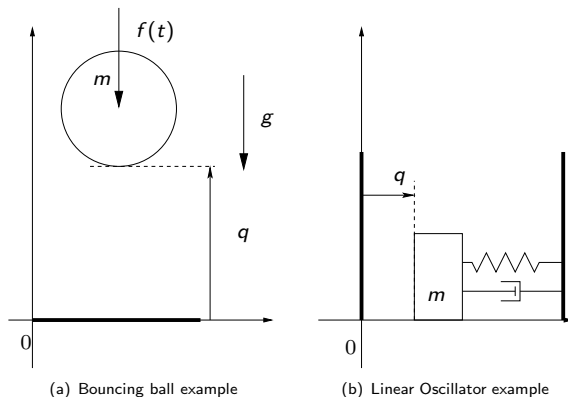


Figure: Academic test examples with analytical solutions

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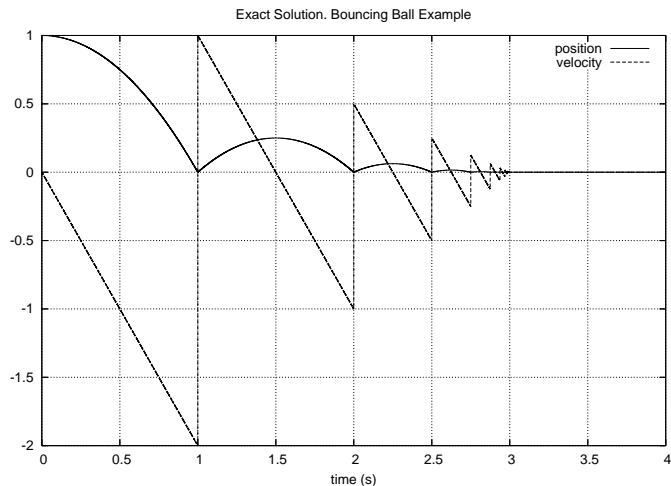


Figure: Analytical solutions. Bouncing ball example]

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Exact Solution. Linear Oscillator Example

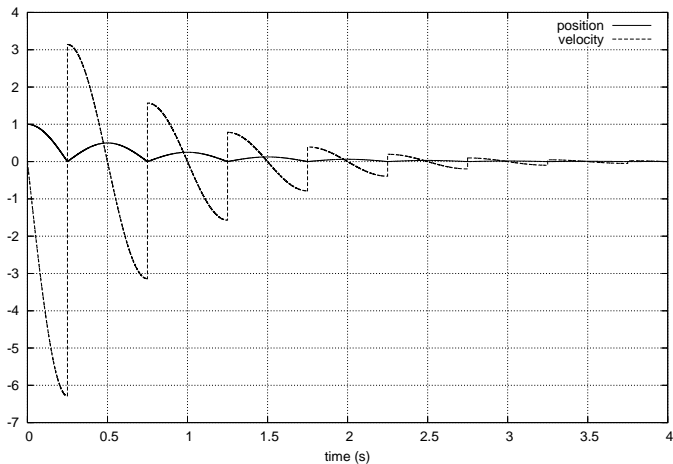


Figure: Analytical solutions. Linear Oscillator

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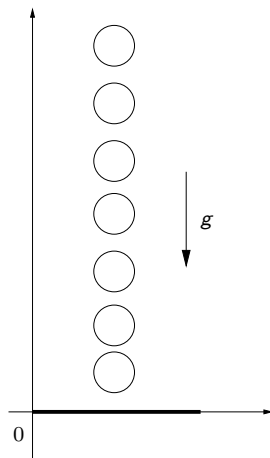
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NonSmooth Multibody Systems (NSMBS)

Academic examples II



(a) N Bouncing balls example

Figure: Academic test examples

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Principle

$$\left\{ \begin{array}{l} M(q_{k+\theta})(v_{k+1} - v_k) - h\tilde{F}_{k+\theta} = G(q_{k+\theta})P_{k+1}, \\ q_{k+1} = q_k + hv_{k+\theta}, \\ U_{k+1} = G^T(q_{k+\theta})v_{k+1} \\ -P_{k+1} \in N_{T_{\mathbb{R}_+^m}(\tilde{y}_{k+\gamma})}(U_{k+1} + eU_k), \\ \tilde{y}_{k+\gamma} = y_k + h\gamma U_k, \quad \gamma \in [0, 1]. \end{array} \right. \quad \begin{array}{l} (9a) \\ (9b) \\ (9c) \\ (9d) \\ (9e) \end{array}$$

with $\theta \in [0, 1]$, $\gamma \geq 0$ and $x_{k+\alpha} = (1 - \alpha)x_{k+1} + \alpha x_k$ and $\tilde{y}_{k+\gamma}$ is a prediction of the constraints.

Schatzman's Time stepping scheme (Paoli and Schatzman, 2002)

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Principle

$$\left\{ \begin{array}{l} M(q_k + 1)(q_{k+1} - 2q_k + q_{k-1}) - h^2 F(t_{k+\theta}, q_{k+\theta}, v_{k+\theta}) = p_{k+1} \quad (10a) \\ v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, \quad (10b) \\ -p_{k+1} \in N_K \left(\frac{q_{k+1} + eq_{k-1}}{1+e} \right), \quad (10c) \end{array} \right.$$

where N_K defined the normal cone to K .

For $K = \{q \in \mathbb{R}^n, y = g(q) \geq 0\}$

$$0 \leq g \left(\frac{q_{k+1} + eq_{k-1}}{1+e} \right) \perp \nabla g \left(\frac{q_{k+1} + eq_{k-1}}{1+e} \right) p_{k+1} \geq 0 \quad (11)$$

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Shared mathematical properties

- ▶ Convergence results for one constraints
- ▶ Convergence results for multiple constraints problems with acute kinetic angles
- ▶ No theoretical proof of order

Mechanical properties

- ▶ Position vs. velocity constraints
- ▶ Respect of the impact in one step (Moreau) vs. Two-steps(Schatzman)
- ▶ Linearized constraints rather than nonlinear.

Convergence in the sense of filled-in graph (Moreau (1978))

$$gr^*(f) = \{(t, x) \in [0, T] \times \mathbb{R}^n, 0 \leq t \leq T \text{ and } x \in [f(t^-), f(t^+)]\}. \quad (12)$$

Such graphs are closed bounded subsets of $[0, T] \times \mathbb{R}^n$, hence, we can use the Hausdorff distance between two such sets with a suitable metric:

$$d((t, x), (s, y)) = \max\{|t - s|, \|x - y\|\}. \quad (13)$$

Defining the excess of separation between two graphs by

$$e(gr^*(f), gr^*(g)) = \sup_{(t,x) \in gr^*(f)} \inf_{(s,y) \in gr^*(g)} d((t, x), (s, y)), \quad (14)$$

the Hausdorff distance between two filled-in graphs h^* is defined by

$$h^*(gr^*(f), gr^*(g)) = \max\{e(gr^*(f), gr^*(g)), e(gr^*(g), gr^*(f))\}. \quad (15)$$

An equivalent grid-function norm to the function norm in \mathcal{L}_1

$$\|e\|_1 = h \sum_{i=0}^N |f_i - f(t_i)| \quad (16)$$

In the same way, the p -norm can be defined by

$$\|e\|_p = \left(h \sum_{i=0}^N |f_i - f(t_i)|^p \right)^{1/p} \quad (17)$$

The computation of this two last norm is easier to implement for piecewise continuous analytical function than the Hausdorff distance.

Global order of convergence.

Definition

A one-step time-integration scheme is of order q for a given norm $\|\cdot\|$ if there exists a constant C such that

$$\|e\| = Ch^q + \mathcal{O}(h^{q+1}) \quad (18)$$

Empirical order of convergence. Moreau's time-stepping scheme

Higher order schemes for nonsmooth mechanical systems.

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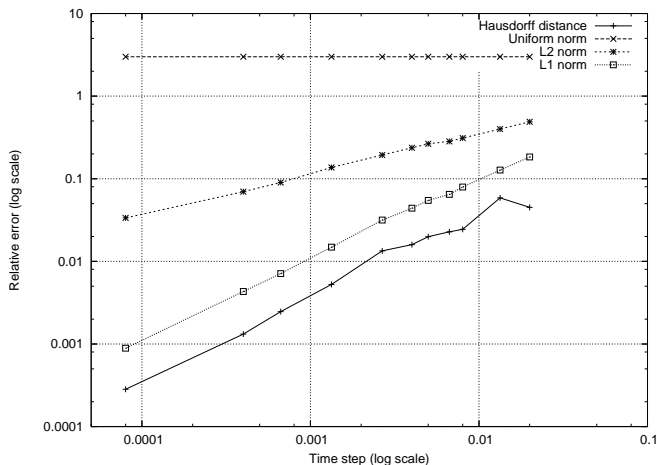
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(a) The bouncing ball example

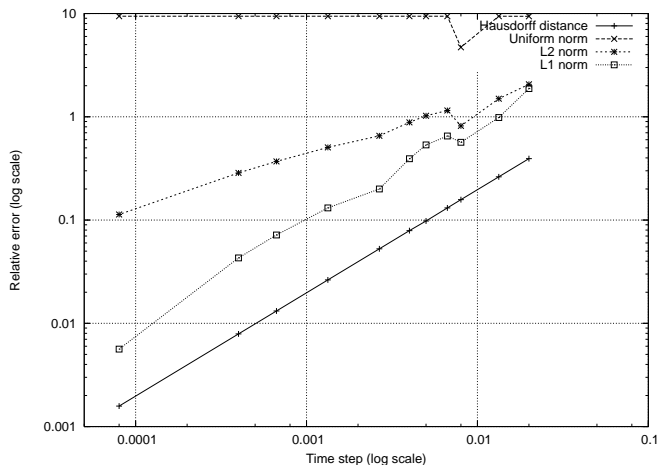
Figure: Empirical order of convergence of the Moreau's time-stepping scheme.

Empirical order of convergence. Moreau's time-stepping scheme

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(a) The linear oscillator example

Figure: Empirical order of convergence of the Moreau's time-stepping scheme.

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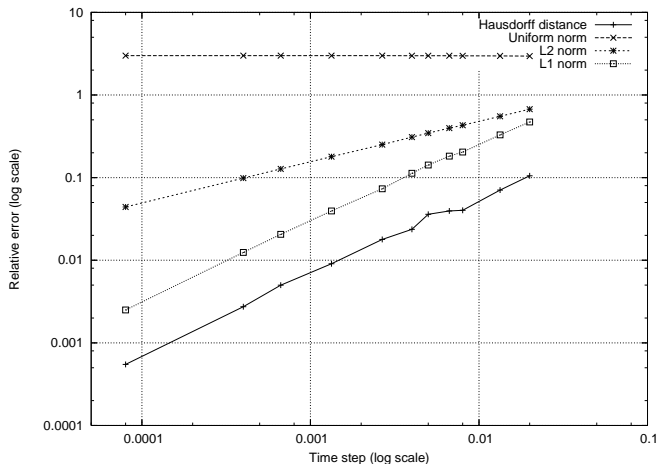
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(a) The bouncing ball example

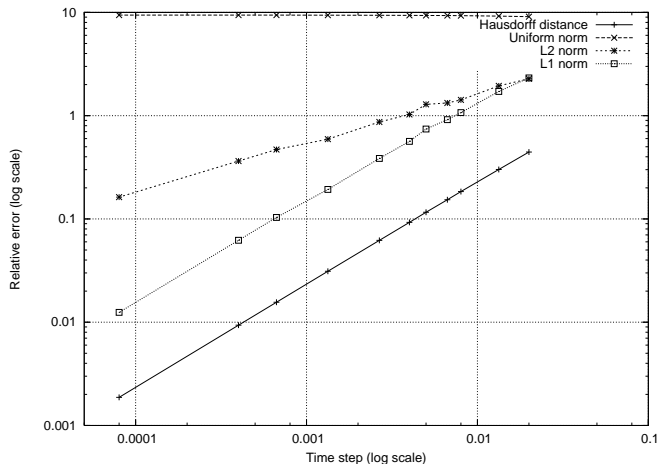
Figure: Empirical order of convergence of the Schatzman–Paoli's time-stepping scheme.

Empirical order of convergence. Schatzman–Paoli's time-stepping scheme

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Notation

$$\mathbf{e} = x(t_k + h) - x_{k+1} = \begin{bmatrix} e_v \\ e_q \end{bmatrix} = \begin{bmatrix} v^+(t_k + h) - v_{k+1} \\ q(t_k + h) - q_{k+1} \end{bmatrix} \quad (19)$$

One impact at time $t_* \in (t_k, t_{k+1}]$

Assumption

$$di = p\delta_{t_*}, \quad \text{or equivalently} \quad dl = P\delta_{t_*}, \quad \text{with } P = G(t_*)p. \quad (20)$$

Notation

$$\mathcal{I} = \{\alpha, \alpha \in \{1..m\}\} \quad (21)$$

$$\mathcal{I}_* = \{\alpha \in \mathcal{I}, P^\alpha \geq 0, U^{\alpha,+}(t_*) - U^{\alpha,-}(t_*) = -(1+e)U^{\alpha,-}(t_*)\} \quad (22)$$

$$\mathcal{I}_p = \{\alpha \in \mathcal{I}, P_{k+1}^\alpha \geq 0, U_{k+1}^\alpha - U_k^\alpha = -(1+e)U_k^\alpha\} \quad (23)$$

Lemma

Let us assume that we have only one elastic impact at time $t_* \in (t_k, t_{k+1}]$ without persistent contact, i.e. , $di = p\delta_{t_*}$.

1. If $\mathcal{I}_* = \mathcal{I}_p$, then the local order of consistency of the scheme is given by

$$\begin{aligned} e_v &= K_v h + \mathcal{O}(h^2) \\ e_q &= K_q h + \mathcal{O}(h^2) \end{aligned} \quad (24)$$

2. If $\mathcal{I}_* \neq \mathcal{I}_p$, then the local order of consistency of the scheme is given by

$$\begin{aligned} e_v &= K_v + \mathcal{O}(h) \\ e_q &= K_q h + \mathcal{O}(h^2) \end{aligned} \quad (25)$$

Local error estimates for the Moreau's time-stepping

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Other cases are treated in the same way

- ▶ *One impact and smooth Lagrange multiplier* The same result holds as in the first Lemma.
- ▶ *losing contact event (take-off) without impact* The order of the time-integration scheme depends on the regularity of the contact forces (at least continuous).
- ▶ *Finite accumulation* The order of the time-integration should be at least 0. Idea of the proof : use the fact that the velocity vanishes and is of bounded variations

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Order "0" case

Standard error estimates do not apply for Order 0.

We propose to extend it to the order 0 of consistency by assuming that the the local error estimate is given by

$$e_{1/2} = 2(x_{1/2} - x_1) + \mathcal{O}(h^2) \quad (26)$$

where x_1 is the result of the time integration with one time-step of length h and $x_{1/2}$ with two time-steps of length $h/2$.

The adaptive time-step control used for smooth ODE is then apply directly Hairer et al. (1993).

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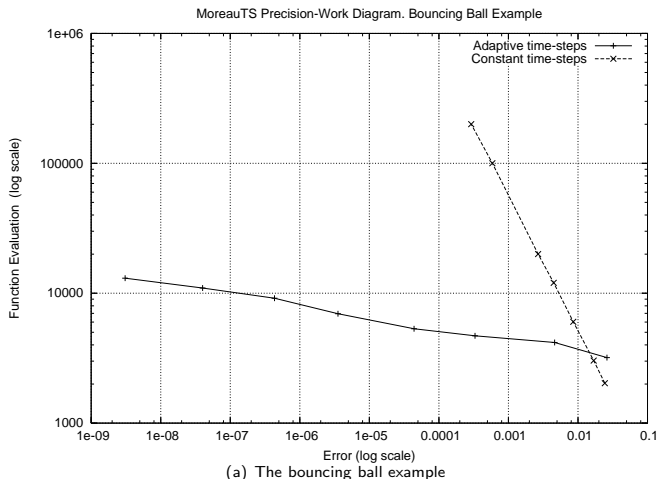


Figure: Precision Work diagram for the Moreau’s time-stepping scheme. Order 0

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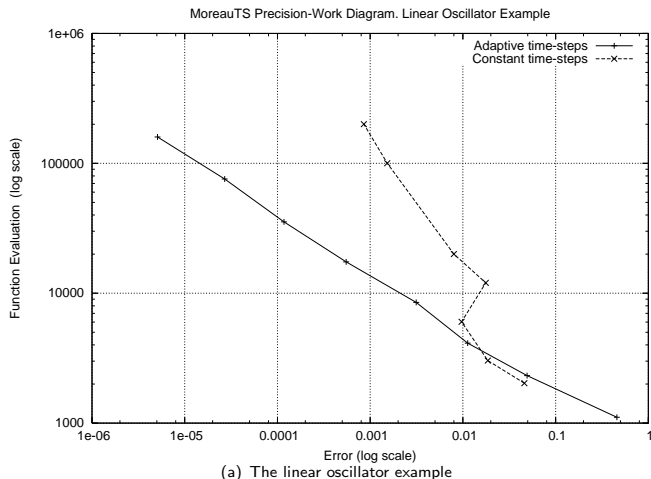


Figure: Precision Work diagram for the Moreau’s time-stepping scheme. Order 0

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Work of Mannshardt (1978) on time-integration schemes of any order for ODE/DAEs with discontinuities (with transversality assumption)

Principle

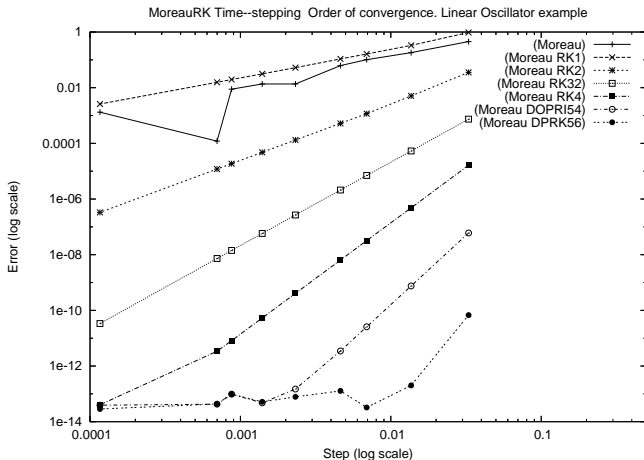
- ▶ Let us assume only one event per time-step at instants t_* .
- ▶ Choose any ODE/DAE solvers of order p
- ▶ Perform a rough location of the event inside the time step of length h
Find an interval $[t_a, t_b]$ such that

$$t_* \in [t_a, t_b] \text{ and } |t_b - t_a| = Ch^{p+1} + \mathcal{O}(h^{p+2}) \quad (27)$$

Dichotomy, Newton, Local Interpolants, Dense output,...

- ▶ Perform an integration on $[t_k, t_a]$ with the ODE solver of order p
- ▶ Perform an integration on $[t_a, t_b]$ with Moreau's time-stepping scheme
- ▶ Perform an integration on $[t_b, t_{k+1}]$ with the ODE solver of order p

Results on the linear oscillator



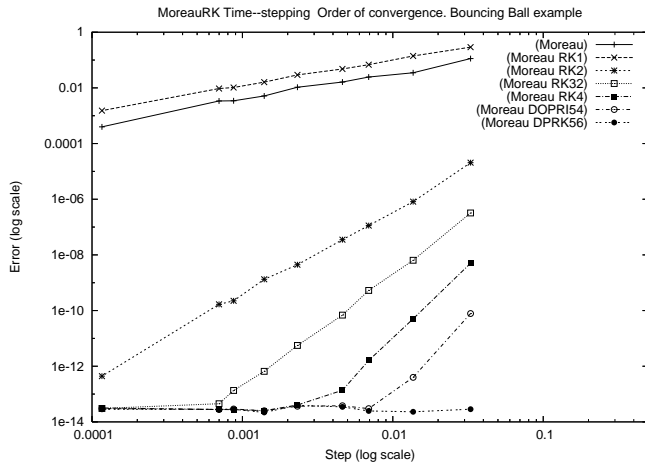
(a) The linear oscillator example

Figure: Precision Work diagram for the Moreau's time-stepping scheme.

Finite accumulation

- ▶ Repeat the whole process on the remaining part of the interval $[t_b, t_k]$
- ▶ By induction, repeat this process up to the end of the original time step.

Results on the Bouncing Ball



(a) The Bouncing Ball example

Figure: Precision Work diagram for the Moreau's time-stepping scheme.

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Adaptive time-step strategies

- ▶ Higher resolution schemes
- ▶ Work with finite accumulation of events

Higher order schemes

- ▶ Schemes of any orders
- ▶ Work with finite accumulation of events

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- ▶ Theoretical works on orders and practical error estimations
Collaborations with people the ODE/DAE communities are welcome.
- ▶ Adaptive time-step strategies on the higher order time-stepping schemes.
- ▶ Improve the pre-detection process of the event and the order of discontinuity
- ▶ Test on nonlinear mechanical systems.
- ▶ Other types of time-stepping schemes (Splitting and time discontinuous Galerkin methods)

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