

Time-integration methods for nonsmooth contact dynamics : beyond the seminal Moreau-Jean scheme

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Introduction

Topic

Dynamics with unilateral contacts (one-sided inequalities)
for finite and infinite freedom dynamics.

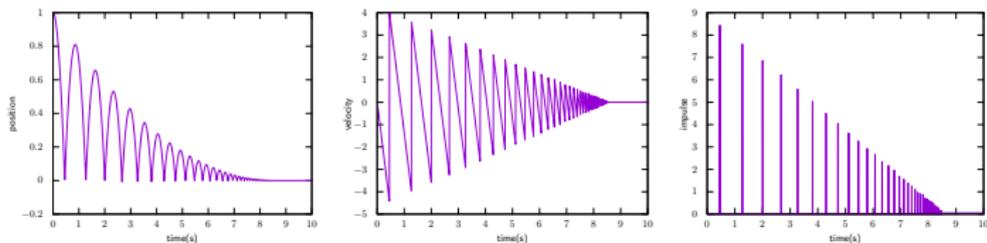
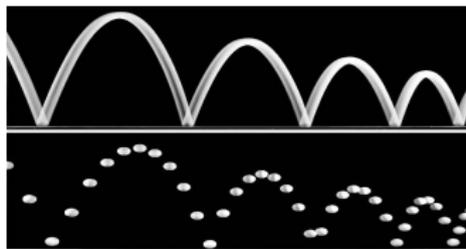
Original motivation: flexible multi-body systems and divided materials.

Objectives

- ▶ Dynamics and unilateral constraints imply nonsmoothness
 - ▶ velocities are discontinuous function of time
 - ▶ possibly, impulsive forces (percussions)
- ▶ Numerical time integration of nonsmooth systems must be done with care
 - ▶ Issues with standard and higher order methods
 - ▶ Moreau–Jean scheme answers to several questions
- ▶ Extensions of Moreau–Jean scheme improve order and qualitative aspects
 - ▶ Focus on nonsmooth generalized α -scheme
- ▶ An open question : nonsmoothness and percussions in elastic solids

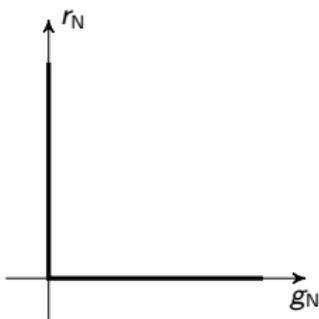
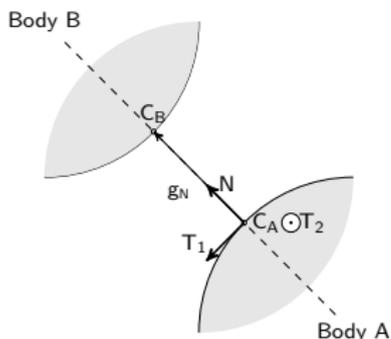
Nonsmooth dynamical systems

nonsmooth = lack of continuity/differentiability



- ▶ nonsmooth solutions in time (jumps, kinks, distributions, measures)
- ▶ nonsmooth modeling and constitutive laws (set-valued mapping, inequality constraints, complementarity, impact laws)

Unilateral contact and impact



- ▶ gap function $g_N = (C_B - C_A)N$.
- ▶ reaction forces
 $r = r_N N + r_T$, $r_N \in \mathbf{R}$ and $r_T \in \mathbf{R}^2$.
- ▶ Signorini condition at position level

$$\begin{aligned}
 0 \leq g_N \perp r_N \geq 0 \\
 \Updownarrow \\
 -r_N \in N_{\mathbf{R}_+}(g_N) \\
 \Updownarrow \\
 r_N = \text{proj}_{\mathbf{R}_+}(r_N - \rho g_N)
 \end{aligned}$$

- ▶ relative velocity
 $u = u_N N + u_T$, $u_N \in \mathbf{R}$ and $u_T \in \mathbf{R}^2$.
- ▶ Signorini condition at velocity level

$$\begin{cases} 0 \leq u_N \perp r_N \geq 0 & \text{if } g_N \leq 0 \\ r_N = 0 & \text{otherwise.} \end{cases}$$

- ▶ Impact law if needed $u_N^+ = -e u_N^-$
 e is the coefficient of restitution.

Multiple constraints

- ▶ $q \in \mathbf{R}^n$ coordinates that describes the state of the system in finite-dimension
- ▶ Notion of admissible set $C(t)$

$$C(t) = \{q \in \mathbf{R}^n, g_\alpha(q, t) \geq 0, \alpha \in \{1 \dots \nu\}\}$$

- ▶ Normal cone inclusion

$$-r \in N_{C(t)}(q)$$

where the normal cone to $C(t)$

$$N_{C(t)}(q) = \{y \mid y = -\nabla_q g_\alpha(q, t) \lambda, \quad 0 \leq g_\alpha(q, t) \perp \lambda_\alpha \geq 0\}$$

- ▶ Coulomb's friction : Second-Order Cone Complementarity condition

$$K^* \ni \hat{u} \perp r \in K \iff -r \in N_{K^*}(\hat{u}) \quad (1)$$

with $K = \{r \in \mathbf{R}^3 \mid \|r_T\| \leq \mu r_n\}$ and $\hat{u} = u + \mu \|u_T\| \mathbf{N}$.

Nonsmooth dynamics in finite dimension.

Space-discretized equations (by FEM, for instance)
or discrete mechanical systems (rigid bodies, linkages, ...)

Definition (Perfect unilateral constraints on the smooth dynamics)

$$\begin{cases} \dot{q} = v \\ M(q) \frac{dv}{dt} + F(t, q, v) = r \\ -r \in N_{C(t)}(q(t)) \end{cases} \quad (2)$$

where r is the generalized force or generalized reaction due to the constraints.

Remark

- ▶ Second order differential inclusion.
- ▶ The unilateral constraints are said to be perfect due to the normality condition.

Nonsmooth dynamics in finite dimension.

Fundamental assumptions.

- ▶ The velocity $v = \dot{q}$ is of Bounded Variations (B.V)
 - The equation are written in terms of a right continuous B.V. (R.C.B.V.) function, v^+ such that

$$v^+ = \dot{q}^+ \quad (3)$$

- ▶ q is related to this velocity by

$$q(t) = q(t_0) + \int_{t_0}^t v^+(t) dt \quad (4)$$

- ▶ The acceleration, (\ddot{q} in the usual sense) is hence a differential measure dv associated with v such that

$$dv(]a, b]) = \int_{]a, b]} dv = v^+(b) - v^+(a) \quad (5)$$

Nonsmooth dynamics in finite dimension.

Definition (Nonsmooth Lagrangian Dynamics)

$$\begin{cases} M(q)dv + F(t, q, v^+)dt = di \\ v^+ = \dot{q}^+ \end{cases} \quad (6)$$

where di is the reaction measure and dt is the Lebesgue measure.

Remarks

- ▶ The nonsmooth Dynamics contains the impact equations and the smooth evolution in a single equation.
- ▶ The formulation allows one to take into account very complex behaviors, especially, finite accumulation (Zeno-state).
- ▶ This formulation is sound from a mathematical Analysis point of view.

References: [19, 20, 15, 16]

Nonsmooth dynamics in finite dimension.

Measures Decomposition

Densities w.r.t. Lebesgue measure dt

$$\frac{dv}{dt} = \gamma = \ddot{q} \quad \text{acceleration defined in the usual sense a.e.}$$

$$\frac{di}{dt} = f \quad \text{Lebesgue measurable force}$$

Densities w.r.t. purely atomic measure $d\nu = \sum_i \delta_{t_i}$

$d\nu$ is a purely atomic measure concentrated at the instants t_i of discontinuities of v

$$\frac{dv}{d\nu} = v^+ - v^- \quad \text{velocity jump}$$

$$\frac{di}{d\nu} = p \quad \text{percussion (impulsive force)}$$

Impact equations and non impulsive dynamics

Using the densities in the nonsmooth Lagrangian Dynamics, one obtains

Definition (Impact equations at any time t_i)

$$M(q)(v^+ - v^-)d\nu = pd\nu, \quad (7)$$

or, equivalently,

$$M(q(t_i))(v^+(t_i) - v^-(t_i)) = p_i, \quad (8)$$

Definition (Smooth Dynamics almost everywhere)

$$M(q)\gamma dt + F(t, q, v)dt = fdt \quad (9)$$

or

$$M(q)\gamma^+ + F(t, q, v^+) = f^+ \quad [dt - a.e.] \quad (10)$$

The Moreau's sweeping process of second order

Definition (Moreau's sweeping process of second order [15, 16])

The inclusion (2) is “replaced” by the following inclusion

$$\begin{cases} M(q)dv + F(t, q, v^+)dt = di \\ v^+ = \dot{q}^+ \\ -di \in N_{T_C(q)}(v^+ + ev^-) \end{cases} \quad (11)$$

Inclusion at the velocity level of the measure

A key stone of this formulation is the inclusion in terms of velocity. For $C = \mathbf{R}_+$,

$$-di \in N_{T_{\mathbf{R}_+}(q)}(v^+ + ev^-) \iff \text{if } q \leq 0, \text{ then } 0 \leq v^+ + ev^- \perp di \geq 0$$

→ Foundation for the Moreau–Jean time–stepping approach.

Mathematical results

Finite dimension

- ▶ Counter example to uniqueness with \mathcal{C}^∞ data (Schatzman, Percivale)
- ▶ Existence and uniqueness in the frictionless case with analytic data (Ballard[3])
- ▶ Frictional case.
 - ▶ No result in the general case
 - ▶ Existence and uniqueness with lumped mass system

Infinite dimension. Elastodynamics (or elasto-plastic) dynamics.

The situation is far more complex. See the discussion at the end of the talk.

Time Integration Schemes

State-of-the-art

Principle of nonsmooth event capturing methods (Time-stepping schemes)

Moreau-Jean's scheme and Schatzman-Paoli's scheme

How to perform numerical time integration ?

1 - Smoothing dynamics

- ▶ Regularization techniques with penalty parameter
- ▶ Advanced and sophisticated methods for FEM discretizations.
 - ▶ Singular mass method and mass redistribution method.
Renard, Laborde and co-workers [14, 18]
 - ▶ Nitsche's method.
Wriggers, Zavarise, Chouly, Hild, Renard among others [23, 11, 12]
- ⊕ convergence proof
- ⊕ enable the use of standard time discretization methods.
- ⊖ numerical stiff ordinary differential equations.
- ⊖ spurious oscillations of contact forces, and then stresses.
- ⊖ issue with inelastic impacts.

How to perform numerical time integration ?

2 - Event detecting schemes (Event-driven)

- ▶ accurate time detection of events
- ▶ standard smooth numerical time integration methods.
- ⊕ higher order integration of free flight motions
- ⊖ sensibility to numerical thresholds
- ⊖ reformulation of constraints at higher kinematic levels.
- ⊖ unable to deal with finite accumulation, or very large number of events.

How to perform numerical time integration ?

3 - Event-capturing schemes (a.k.a. time stepping schemes)

- ⊕ robust, stable and proof of convergence
- ⊕ low kinematic level for the constraints
- ⊕ able to deal with finite accumulation
- ⊖ very low order of accuracy even in free flight motions
- ⊖ drift of the constraints at position, velocity or acceleration levels.

Main schemes

- ▶ Moreau–Jean
- ▶ Schatzman–Paoli

Principle of nonsmooth event capturing methods (Time-stepping schemes)

1. A unique formulation of the dynamics is considered. For instance, a dynamics in terms of measures.

$$\begin{cases} -mdv + fdt = di \\ \dot{q} = v^+ \\ 0 \leq di \perp v^+ \geq 0 \text{ if } q \leq 0 \end{cases} \quad (12)$$

2. The time-integration is based on a consistent approximation of the equations in terms of measures. For instance,

$$\int_{]t_k, t_{k+1}] } dv = \int_{]t_k, t_{k+1}] } dv = (v^+(t_{k+1}) - v^+(t_k)) \approx (v_{k+1} - v_k) \quad (13)$$

3. Consistent approximation of measure inclusion.

$$0 \leq di \perp v^+ \geq 0 \text{ if } q \leq 0 \quad \rightarrow \quad \begin{cases} p_{k+1} \approx \int_{]t_k, t_{k+1}] } di \\ 0 \leq p_{k+1} \perp v_{k+1} \geq 0 \text{ if } \tilde{q}_k \leq 0 \end{cases} \quad (14)$$

Moreau–Jean’s Time stepping scheme [16, 13]

Principle

$$\left\{ \begin{array}{l} M(q_{k+\theta})(v_{k+1} - v_k) - hF_{k+\theta} = p_{k+1} = G(q_{k+\theta})P_{k+1}, \\ q_{k+1} = q_k + hv_{k+\theta}, \\ u_{k+1} = G^T(q_{k+\theta})v_{k+1} \\ \begin{array}{ll} 0 \leq u_{k+1}^\alpha + eU_k^\alpha \perp P_{k+1}^\alpha \geq 0 & \text{if } \bar{g}_{k,\gamma}^\alpha \leq 0 \\ P_{k+1}^\alpha = 0 & \text{otherwise} \end{array} \end{array} \right. \quad \begin{array}{l} (15a) \\ (15b) \\ (15c) \\ (15d) \end{array}$$

with

- ▶ $G(q) = \nabla_q g(q)$
- ▶ $\theta \in [0, 1]$
- ▶ $x_{k+\theta} = (1 - \theta)x_{k+1} + \theta x_k$
- ▶ $F_{k+\theta} = F(t_{k+\theta}, q_{k+\theta}, v_{k+\theta})$
- ▶ $\bar{g}_{k,\gamma} = g_k + \gamma h u_k, \gamma \geq 0$ is a prediction of the constraints.

Schatzman–Paoli’s Time stepping scheme [17]

Principle

$$\left\{ \begin{array}{l} M(q_{k+1})(q_{k+1} - 2q_k + q_{k-1}) - h^2 F_{k+\theta} = p_{k+1}, \end{array} \right. \quad (16a)$$

$$\left\{ \begin{array}{l} v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, \end{array} \right. \quad (16b)$$

$$\left\{ \begin{array}{l} -p_{k+1} \in N_K \left(\frac{q_{k+1} + eq_{k-1}}{1+e} \right), \end{array} \right. \quad (16c)$$

where N_K defined the normal cone to K .

For $K = \{q \in \mathbf{R}^n, y = g(q) \geq 0\}$

$$0 \leq g \left(\frac{q_{k+1} + eq_{k-1}}{1+e} \right) \perp \nabla g \left(\frac{q_{k+1} + eq_{k-1}}{1+e} \right) p_{k+1} \geq 0 \quad (17)$$

But ...

Both schemes are

- ▶ quite inaccurate (at most first order)
- ▶ “conserve” or “dissipate” a lot of energy

This is a consequence of the first order approximation of the smooth forces term F

Recent improvements

- ▶ Time discontinuous Galerkin methods, with T. Schindler et al. [21, 22]
- ▶ Stabilized index-2 formulation [2, 1]
- ▶ Stabilized index-1 formulation, with O. Brüls and A. Cardona [5]
- ▶ Time finite element method and variational integrators. G. Cappobianco, S. Eugster et al.[7, 6]
- ▶ Nonsmooth generalized- α schemes, with O. Brüls, A. Cardona et al. [10, 4, 8]

Nonsmooth generalized- α schemes

Direct application of Newmark scheme or generalized α -scheme

Splitting the dynamics between smooth and nonsmooth part

GGL stabilization

Numerical illustrations

Direct application of Newmark scheme or generalized α -scheme

Inconsistent results in discrete time with a direct application

- ▶ Contact condition at velocity level is wrong
- ▶ Pseudo-artificial impact law.
- ▶ Contact stresses are polluted with spurious oscillations.

Do not directly apply generalized α -scheme with unilateral contact !!

The nonsmooth generalized α scheme

Splitting the dynamics between smooth and nonsmooth part

$$d\mathbf{w} = d\mathbf{v} - \dot{\tilde{\mathbf{v}}} dt \quad (18)$$

Smooth (non-impulsive) part

Solutions of the following DAE

$$\dot{\tilde{\mathbf{q}}} = \tilde{\mathbf{v}} \quad (19a)$$

$$\mathbf{M}(\mathbf{q}) \dot{\tilde{\mathbf{v}}} - \mathbf{g}_{\mathbf{q}}^T(\mathbf{q}) \tilde{\boldsymbol{\lambda}} = \mathbf{f}(\mathbf{q}, \mathbf{v}, t) \quad (19b)$$

$$\mathbf{g}_{\mathbf{q}}^{\bar{\mathcal{U}}}(\mathbf{q}) \tilde{\mathbf{v}} = \mathbf{0} \quad (19c)$$

$$\tilde{\boldsymbol{\lambda}}^{\mathcal{U}} = \mathbf{0} \quad (19d)$$

with the initial value $\tilde{\mathbf{v}}(t_n) = \mathbf{v}(t_n)$, $\tilde{\mathbf{q}}(t_n) = \mathbf{q}(t_n)$.

The nonsmooth generalized α scheme

Splitting the dynamics between smooth and nonsmooth part

$$\dot{\mathbf{q}} = \mathbf{v} \quad (20a)$$

$$d\mathbf{v} = d\mathbf{w} + \dot{\hat{\mathbf{v}}} dt \quad (20b)$$

$$\mathbf{M}(\mathbf{q}) \dot{\hat{\mathbf{v}}} - \mathbf{g}_{\mathbf{q}}^{\bar{\mathcal{U}}, T} \tilde{\lambda}^{\bar{\mathcal{U}}} = \mathbf{f}(\mathbf{q}, \mathbf{v}, t) \quad (20c)$$

$$\mathbf{g}_{\mathbf{q}}^{\bar{\mathcal{U}}} \tilde{\mathbf{v}} = \mathbf{0} \quad (20d)$$

$$\tilde{\lambda}^{\mathcal{U}} = \mathbf{0} \quad (20e)$$

$$\mathbf{M}(\mathbf{q}) d\mathbf{w} - \mathbf{g}_{\mathbf{q}}^T (d\mathbf{i} - \tilde{\lambda} dt) = \mathbf{0} \quad (20f)$$

$$\mathbf{g}_{\mathbf{q}}^{\bar{\mathcal{U}}} \mathbf{v} = \mathbf{0} \quad (20g)$$

$$\text{if } g^j(\mathbf{q}) \leq 0 \text{ then } 0 \leq g_{\mathbf{q}}^j \mathbf{v} + e g_{\mathbf{q}}^j \mathbf{v}^- \perp d i^j \geq 0, \quad \forall j \in \mathcal{U} \quad (20h)$$

The nonsmooth generalized α scheme

GGL approach to stabilize the constraints at the position level

The equations of motion become

$$\mathbf{M}(\mathbf{q}) \dot{\mathbf{q}} - \mathbf{g}_{\mathbf{q}}^T \boldsymbol{\mu} = \mathbf{M}(\mathbf{q}) \mathbf{v} \quad (21a)$$

$$\dot{\mathbf{q}} \rightarrow \mathbf{g}^{\bar{u}}(\mathbf{q}) = \mathbf{0} \quad (21b)$$

$$\mathbf{0} \leq \mathbf{g}^{\mathcal{U}}(\mathbf{q}) \perp \boldsymbol{\mu}^{\mathcal{U}} \geq \mathbf{0} \quad (21c)$$

$$d\mathbf{v} = d\mathbf{w} + \dot{\tilde{\mathbf{v}}} dt \quad (21d)$$

$$\mathbf{M}(\mathbf{q}) \dot{\tilde{\mathbf{v}}} - \mathbf{g}_{\mathbf{q}}^{\bar{u},T} \tilde{\boldsymbol{\lambda}}^{\bar{u}} = \mathbf{f}(\mathbf{q}, \mathbf{v}, t) \quad (21e)$$

$$\mathbf{g}_{\mathbf{q}}^{\bar{u}} \tilde{\mathbf{v}} = \mathbf{0} \quad (21f)$$

$$\tilde{\boldsymbol{\lambda}}^{\mathcal{U}} = \mathbf{0} \quad (21g)$$

$$\mathbf{M}(\mathbf{q}) d\mathbf{w} - \mathbf{g}_{\mathbf{q}}^T (d\mathbf{i} - \tilde{\boldsymbol{\lambda}} dt) = \mathbf{0} \quad (21h)$$

$$\mathbf{g}_{\mathbf{q}}^{\bar{u}} \mathbf{v} = \mathbf{0} \quad (21i)$$

$$\text{if } \mathbf{g}^j(\mathbf{q}) \leq 0 \text{ then } \mathbf{0} \leq \mathbf{g}_{\mathbf{q}}^j \mathbf{v} + \mathbf{e} \mathbf{g}_{\mathbf{q}}^j \mathbf{v}^- \perp d\mathbf{i}^j \geq 0, \quad \forall j \in \mathcal{U} \quad (21j)$$

The nonsmooth generalized α scheme

Velocity jumps and position correction

The multipliers $\Lambda(t_n; t)$ and $\nu(t_n; t)$ are defined as

$$\Lambda(t_n; t) = \int_{(t_n, t]} (d\mathbf{i} - \tilde{\lambda}(\tau) d\tau) \quad (22a)$$

$$\nu(t_n; t) = \int_{t_n}^t (\boldsymbol{\mu}(\tau) + \Lambda(t_n; \tau)) d\tau \quad (22b)$$

with $\Lambda(t_n; t_n) = \nu(t_n; t_n) = \mathbf{0}$.

The velocity jump and position correction variables

$$\mathbf{W}(t_n; t) = \int_{(t_n, t]} d\mathbf{w} = \mathbf{v}(t) - \tilde{\mathbf{v}}(t) \quad (23a)$$

$$\mathbf{U}(t_n; t) = \int_{t_n}^t (\dot{\mathbf{q}} - \tilde{\mathbf{v}}) dt = \mathbf{q}(t) - \tilde{\mathbf{q}}(t) \quad (23b)$$

- Low-order approximation of impulsive terms.
- Higher-order approximation of non impulsive terms.

The nonsmooth generalized α scheme

$$\mathbf{M}(\mathbf{q}_{n+1})\mathbf{U}_{n+1} - \mathbf{g}_{\mathbf{q},n+1}^T \boldsymbol{\nu}_{n+1} = \mathbf{0} \quad (24a)$$

$$\mathbf{g}^{\bar{\mathcal{U}}}(\mathbf{q}_{n+1}) = \mathbf{0} \quad (24b)$$

$$\mathbf{0} \leq \mathbf{g}^{\mathcal{U}}(\mathbf{q}_{n+1}) \perp \boldsymbol{\nu}_{n+1}^{\mathcal{U}} \geq \mathbf{0} \quad (24c)$$

$$\mathbf{M}(\mathbf{q}_{n+1})\dot{\tilde{\mathbf{v}}}_{n+1} - \mathbf{f}(\mathbf{q}_{n+1}, \mathbf{v}_{n+1}, t_{n+1}) - \mathbf{g}_{\mathbf{q},n+1}^{\bar{\mathcal{U}}, T} \tilde{\boldsymbol{\lambda}}_{n+1}^{\bar{\mathcal{U}}} = \mathbf{0} \quad (24d)$$

$$\mathbf{g}_{\mathbf{q},n+1}^{\bar{\mathcal{U}}} \tilde{\mathbf{v}}_{n+1} = \mathbf{0} \quad (24e)$$

$$\mathbf{M}(\mathbf{q}_{n+1})\mathbf{W}_{n+1} - \mathbf{g}_{\mathbf{q},n+1}^T \boldsymbol{\Lambda}_{n+1} = \mathbf{0} \quad (24f)$$

$$\mathbf{g}_{\mathbf{q},n+1}^{\bar{\mathcal{U}}} \mathbf{v}_{n+1} = \mathbf{0} \quad (24g)$$

$$\text{if } g^j(\mathbf{q}_{n+1}^*) \leq 0 \text{ then } 0 \leq g_{\mathbf{q},n+1}^j \mathbf{v}_{n+1} + e g_{\mathbf{q},n}^j \mathbf{v}_n \perp \boldsymbol{\Lambda}_{n+1}^j \geq 0, \forall j \in \mathcal{U}$$

The nonsmooth generalized α scheme

Nonsmooth generalized α -scheme

$$\tilde{\mathbf{q}}_{n+1} = \mathbf{q}_n + h\mathbf{v}_n + h^2(0.5 - \beta)\mathbf{a}_n + h^2\beta\mathbf{a}_{n+1} \quad (25a)$$

$$\mathbf{q}_{n+1} = \tilde{\mathbf{q}}_{n+1} + \mathbf{U}_{n+1} \quad (25b)$$

$$\tilde{\mathbf{v}}_{n+1} = \mathbf{v}_n + h(1 - \gamma)\mathbf{a}_n + h\gamma\mathbf{a}_{n+1} \quad (25c)$$

$$\mathbf{v}_{n+1} = \tilde{\mathbf{v}}_{n+1} + \mathbf{W}_{n+1} \quad (25d)$$

$$(1 - \alpha_m)\mathbf{a}_{n+1} + \alpha_m\mathbf{a}_n = (1 - \alpha_f)\dot{\tilde{\mathbf{v}}}_{n+1} + \alpha_f\dot{\tilde{\mathbf{v}}}_n \quad (25e)$$

Special cases

- ▶ $\alpha_m = \alpha_f = 0 \rightarrow$ Nonsmooth Newmark
- ▶ $\alpha_m = 0, \alpha_f \in [0, 1/3] \rightarrow$ Nonsmooth Hilber-Hughes-Taylor (HHT)

Spectral radius at infinity $\rho_\infty \in [0, 1]$

$$\alpha_m = \frac{2\rho_\infty - 1}{\rho_\infty + 1}, \quad \alpha_f = \frac{\rho_\infty}{\rho_\infty + 1}, \quad \beta = \frac{1}{4}\left(\gamma + \frac{1}{2}\right)^2. \quad (26)$$

The nonsmooth generalized α scheme

Observed properties on examples

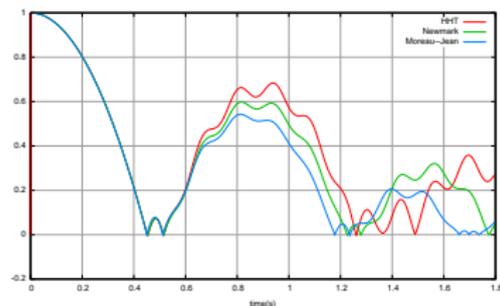
- ▶ the scheme is consistent and globally of order one.
- ▶ the scheme seems to share the stability property as the original HHT
- ▶ the scheme dissipates energy only in high-frequency oscillations (w.r.t the time-step.)

Discrete energy balance (proof in [2])

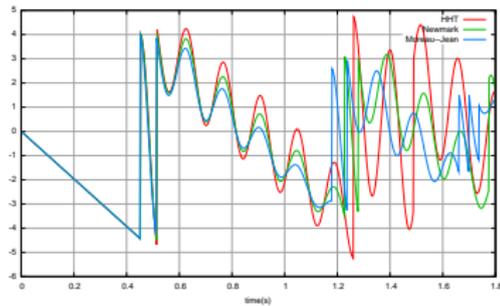
- ▶ For the Moreau-Jean, a simple variant allows us to obtain a scheme which always dissipates energy.
 - ▶ For the Newmark and the HHT scheme with retrieve the dissipation properties as the smooth case. The term associated with impact is added in the balance.
- nonsmooth generalized- α -schemes are stable with a controllable dissipation of mechanical energy and satisfies kinematic constraints at various levels

Numerical Illustrations

Two ball oscillator with impact.



Position of the first ball



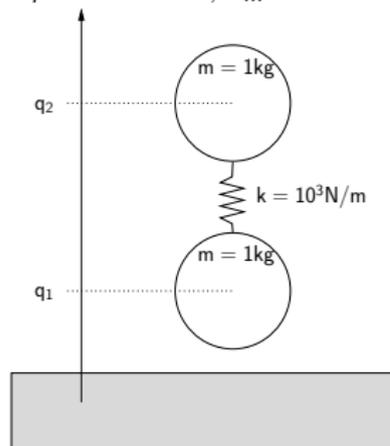
Velocity of the first ball

Time-step : $h = 2e - 3$.

Moreau ($\theta = 1.0$).

Newmark ($\gamma = 1.0, \beta = 0.5,$
 $\alpha_m = \alpha_f = 0$).

HHT ($\gamma = 1.0, \beta = 0.5,$
 $\alpha_f = 0.1, \alpha_m = 0$)



Numerical Illustrations

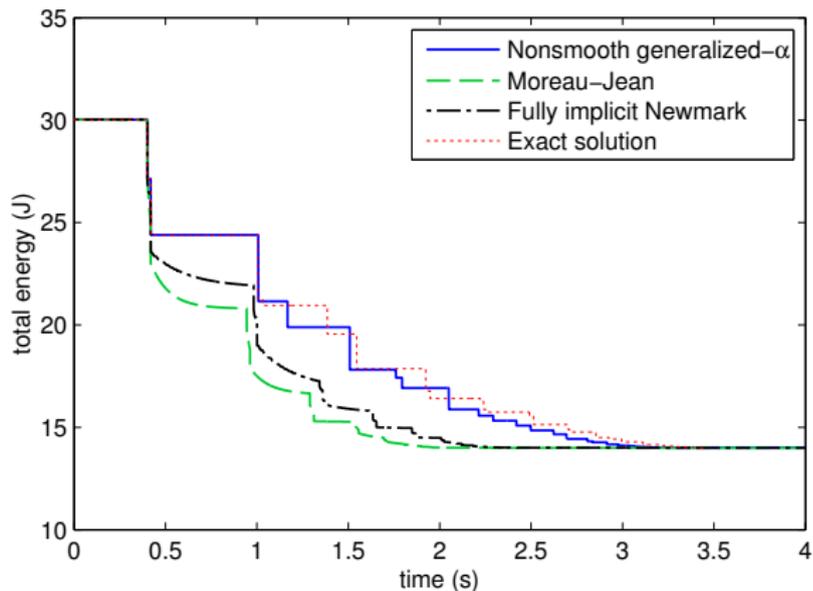
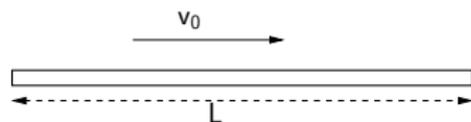


Figure 7. Numerical results for the total energy of the bouncing oscillator.

Numerical Illustrations

Impacting elastic bar



$$g_3(\mathbf{q}) = x_1 \geq 0$$

$$e = 0.0$$

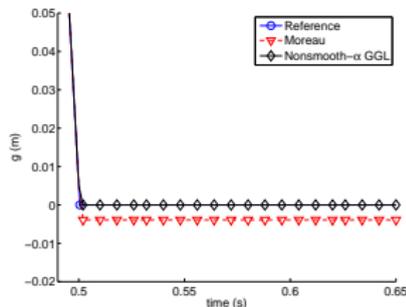
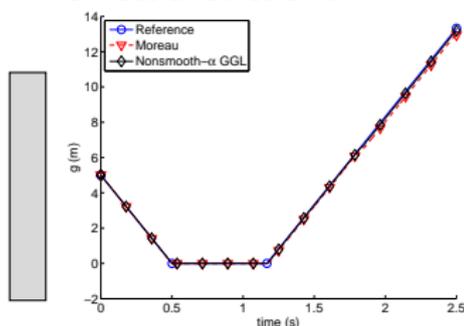
200 finite elements

Time-step : $h = 2e - 3$.

Moreau ($\theta = 1/1.8$).

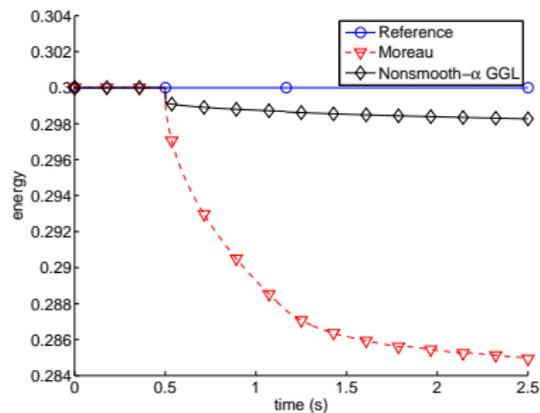
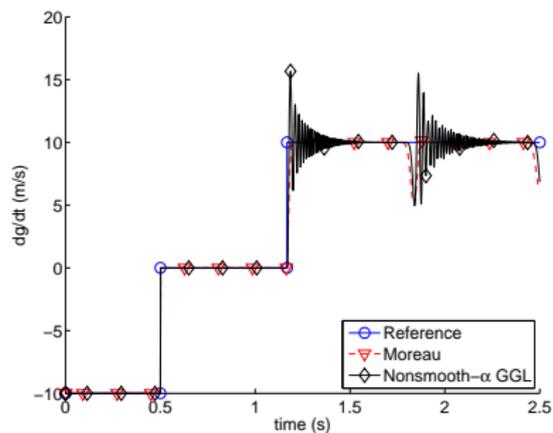
α -schemes ($\rho_\infty = 0.8$)

Unilateral constraint



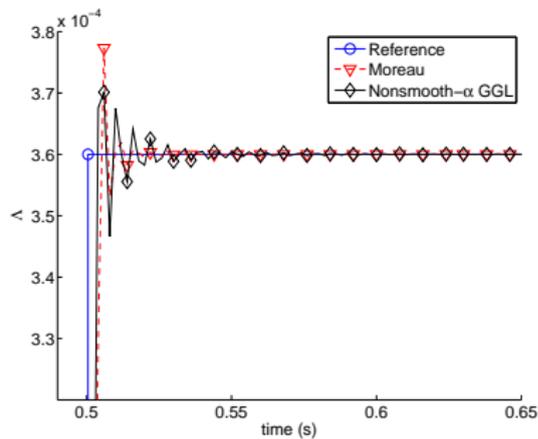
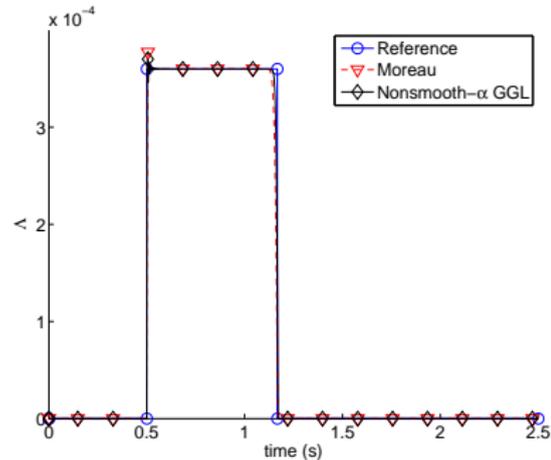
Numerical Illustrations

Impacting elastic bar



Numerical Illustrations

Impacting elastic bar



Open discussion: Nonsmoothness and percussions in continuum media

A modeling problem



Standard assumptions in continuum mechanics

- ▶ Unilateral contact in elastic solids generates traveling surfaces (manifold of co-dimension 1) of velocity discontinuities

$$\mathcal{S} = \{x, t \in \Omega \times [0, T] \mid \mathbf{v}^+(x, t) \neq \mathbf{v}^-(x, t)\}$$

- ▶ Discontinuity surfaces have no mass (negligible sets with respect to the mass measure (no discrete mass))
Theory of shock waves in continuum media. Germain et al.
- ▶ The conservation equation and principles of virtual power implies that is no impulsive stresses or forces. Virtual power of inertial forces at time of jump t

$$\int_{\Omega} \frac{\mathbf{v}^{*,+}(x, t) + \mathbf{v}^{*, -}(x, t)}{2} \cdot (\mathbf{v}^+(x, t) - \mathbf{v}^-(x, t)) dm = 0$$

Mathematical results

Few generic mathematical results

- ▶ 1D, 2D, or 3D elastic half-spaces, or tubes:
 - ▶ Existence and uniqueness obtained by Lebeau and Schatzman
 - ▶ Conservation of energy is obtained (and not imposed).
 - ▶ No impact law in the models.

General implicit assumption

No impulsive forces and no need of impact law for closing the system.

Consequences

- ▶ Impact law in space-discretized systems should not change the results at convergence in time and space
- ▶ Coefficient of restitution acts as a numerical parameter that is convenient in discrete time and space.

Mathematical results

but, because there is a but

Quote from the Lebeau and Schatzman's article :

There seems to be a great difference between unilateral constraints on an open subset of Ω and on a submanifold of lower dimension of Ω .

$\Omega = \{x \in \mathbf{R}^d, x_d > 0\}$ is the ambient half-space of study

Mathematical results

Submanifold of lower dimension : strings, beams, plates and shells

The solutions are far more complicated and raise modeling issues.

- ▶ Strings (1D wave equation) (Cabannes, Schatzman et al.)
 - ▶ punctual obstacles: no impulsive forces
 - ▶ convex and concave obstacle : possible impulse force and the need for an impact law or a conservation of energy rule
- ▶ Beams
 - ▶ Paoli and Shillor: Existence of solutions for a clamped beam with two stop at free end.
 - ▶ Reaction forces are impulsive.
 - ▶ no uniqueness : an ingredient is missing ?
- ▶ distributed discrete masses

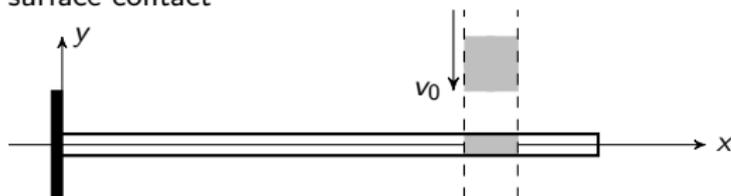
Consequences

- ▶ An impact law, of conservation law, may be needed in the model.
- ▶ Coefficient of restitution is no longer a numerical parameter , and should influence the results at convergence.

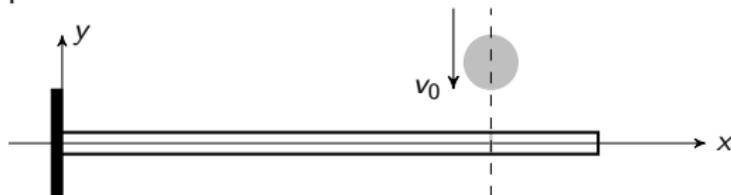
Some illustrations

Impact on a cantilever beam

- ▶ surface contact



- ▶ punctual contact



Chatterjee's work [9]

Response of infinite beam to a punctual impulse by Fourier transform

Elastic infinite beams show velocity discontinuity for the whole beam at initial time .
(infinite speed of bending wave)

$$-u_{tt} + \alpha u_{xxxx} = p$$

Conclusions

- ▶ Space discretized systems are finite dimensional systems :
 - ▶ Moreau-Jean scheme deals consistently with nonsmoothness
 - ▶ impact law or velocity level constraints is a good stabilization technique (index-reduction)
 - ▶ coefficient of restitution is a useful numerical parameter
- ▶ Nonsmooth generalized α -scheme extends all the good properties of original schemes (both Moreau–Jean and generalized α)
- ▶ If the continuous model needs for an impact law, the discrete scheme can take into account this feature, otherwise it enables stabilization of the constraints.
- ▶ For multi-body systems (flexible+rigid+joints+contact+friction), we have a monolithic scheme that is consistent.

Thank you for your attention.

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